A Solid-State Operational Amplifier of High Stability

DC AMPLIFIERS play a role of great importance in instrumentation where they permit observation of low-level potentials not only from regular electrical sources but from mechanical, chemical and biological sources as well. In analog computer work these amplifiers are used to simulate mathematical operations such as integration and summing. They are also invaluable for increasing the sensitivity of voltmeters and recorders, or isolating them from the signal source. For all of these applications, though, the amplifier must have a high degree of gain stability and very low intrinsic voltage- or current-offset to permit the accurate observation of the desired signal.

A new dc amplifier has been designed which achieves greater reliability and accuracy than previously available in a solid state device of this type. A maximum drift level of 1 microvolt per week at constant temperature and a temperature coefficient of but one-half microvolt per °C with a 100 kilohm summing point impedance constitute an order of magnitude improvement over previous all-solid-state dc amplifiers. The amplifier is designed with plug-in modules that permit a wide variety of applications. It has a gain stability of ±.01% per week, is extremely reliable, and is unaffected by mounting position or external vibration, as no mechanical choppers or vacuum tubes are used.

Fig. 1. New solid-state dc amplifiers (group of five in case at left) have high stability, low drift, fast recovery on large overloads, and use panel plug-in modules to adapt to many uses. Unit is produced by Hp's Dymec division.

Fig. 2. Basic circuit arrangement of new amplifier. Feedback impedances are in plug-ins to permit a variety of uses for amplifier.
Special attention has also been paid to overload recovery time which is of vital importance in commutated systems. In such a system, an overload voltage for a particular channel may place a slow-recovery-time amplifier out of operation for several succeeding channels, and thereby lose important data. In the new amplifier recovery time is shorter than 1 millisecond in most cases with input overloads as high as 300 volts.

The amplifier has a self-contained power supply which requires only 4 watts of ac power, resulting in negligible internal temperature rise, and is encased in a compact modular cabinet suitable for both rack and bench use. A combining case that holds up to 6 of the amplifiers in an overall height of but 7 inches permits the amplifiers to be carried or installed in a rack or used on a bench.

**PLUG-IN FUNCTION SELECTION**

The basic circuit arrangement of the amplifier is shown in Fig. 2. The feedback impedances $Z_f$ and $Z_s$ are located in plug-in units which thus determine the overall characteristics of the amplifier. In three of the plug-in units the feedback impedances have been selected to give the amplifier the gains and bandwidths listed elsewhere herein. In the fourth unit jacks are provided on the unit panel so that the user can merely plug in the impedances that will give a desired operational mode for the amplifier. For example, to integrate an electrical signal a resistor would be used for $Z_s$, and a capacitor for $Z_f$.

The forward transfer function $E_o/E_i$ is the ratio of $Z_f$ to $Z_s$, a relation which occurs when the amplifier gain $K$ and input impedance are very large, and the output impedance is small. The new amplifier more than meets these requirements since its nominal dc gain is 100 million, its input resistance is above 1 megohm, and its output impedance is less than 10 ohms. The open-loop roll-off has been held to no more than 6 db per octave to achieve stable operation with a variety of transfer functions.

**OVERLOAD RECOVERY**

In data acquisition systems, rapid recovery from input signals that greatly exceed the dynamic range of the instrument is a prime amplifier requisite. As discussed in the circuitry section, the chopper amplifier is designed to recover from overload quickly by obtaining its low frequency pole by feedback, rather than using a passive RC time constant. Another factor in providing
the rapid overload recovery time obtained in the DY-2460A is a special circuit which automatically lowers the gain when the output exceeds a certain voltage level.

This is accomplished by Zener diodes in the overload circuit (Fig. 6) which are turned on for outputs greater than ±10.5 volts. They allow current to flow to the summing point to balance out the current from the signal source, which keeps the summing point at essentially zero volts. This has the same effect as shorting the output of the amplifier to the input and reducing the gain to zero. The amplifier phase response has been carefully controlled to permit doing this without instability, as the system under these conditions has 160 db of loop gain.

With inputs up to 300 volts the overload circuit will prevent the amplifier from saturating with any gain setting for the M1 and M2 plug-in. Total recovery time (Fig. 4) then consists of 20 μs to turn off the overload circuit, plus the step response time of the amplifier to go from the limited output of 10.5 volts to zero which is a function of gain setting (½ millisecond to settle to 0.1% for the M1 plug-in at a gain of 100). Additional diodes in the overload circuit prevent the Zener leakage current from altering the gain of the amplifier in its linear region and reducing the ±.01% linearity specification. In cases where the input exceeds 300 volts, clamp-

**AMPLIFIER PLUG-INS**

To adapt the new amplifier to a wide range of applications, four plug-in units have been designed. These units contain the feedback and input impedances $Z_f$ and $Z_s$ as described elsewhere in this article, and therefore determine the transfer function of the amplifier. The plug-ins fit into a recess in the front panel and are secured by a thumb-screw.

**DATA AMPLIFIER PLUG-INS**

The data systems plug-in M1 was designed for data acquisition systems where precise dc gains are needed. In addition to five gain positions between 10 and 10000, a ×0 (shorted output) position is also provided. A front panel control with a range of ±2% trims the gain to the desired accuracy. A large amount of negative feedback is used (approximately 100 db at a forward gain of 1000) to make the amplifier characteristics essentially dependent on the feedback elements only. Through the use of high quality resistors, the M1 unit has a gain stability of ±.01% per week and is linear to ±.01% under maximum load. Fast settling time permits rapid multiplexing in data systems; for example, the output reaches 0.1% of its final value in less than 250 microseconds at a gain of 100. Overload recovery is also fast, being 20 μs plus the amplifier settling time (which is a function of gain) for inputs up to 300 volts peak at any gain setting.

A unit which offers bench use convenience in that front panel input and output as well as rear panel connectors are provided is the M2 plug-in. Any gain setting between 1 and 11000 can be obtained by its control arrangement consisting of a 10-turn potentiometer and dial along with the ×1 through ×1000 decade multiplier. Gain stability, linearity, settling time, and overload recovery time are the same as the M1 unit.

**OPERATIONAL PLUG-IN**

For using the amplifier in its operational sense (i.e., as a mathematical operator) the M3 patch unit plug-in is useful. Front panel terminals are provided for the feedback impedance and up to three input impedances, as well as three input, output, and ground connections. Integrators, non-linear shaping networks, summers, and multipliers may be easily constructed by inserting the proper components, or several amplifiers may be patched together as an analog computer. The three inputs and the output are also available on the rear connector plug.

**ISOLATION PLUG-IN**

For applications where extreme isolation is needed between source and load the M4 plus-one unit offers an input impedance of greater than 10$^{10}$ ohms and 300 kc bandwidth. With a 100K load the dc gain is accurate to two parts in a million; which, for example, would allow its use as a buffer amplifier for a voltage standard. The ac gain accuracy is also high, being ±.1% at 1 kc.
ing diodes are provided at the sum-
mimg point to prevent amplifier
damage.

**PHOTOCONDUCTOR CHOPPER**

In order to make the amplifier well-suited to use in the microvolt region, a chopper amplifier for low frequency signals precedes the main amplifier. The chopper amplifier (K3 in Fig. 6) modulates the dc and low frequency signals, amplifies them in an ac-coupled amplifier, and reconstructs the original signal in the demodulator for a dc-to-dc gain of $10^4$. In a system like this the only location where dc offset is significant is in the input modulator or chopper circuit. Any drift occurring after the chopper amplifier is divided by $10^4$ when the offset is referred to the input.

The design of dc amplifiers using chopper stabilization has advanced rapidly in the past few years with the use of solid-state components; but in cases where drift must be kept to a low level, mechanical choppers have still provided the best solution up to now. However, the use of photoconductor choppers, which -hp- has successfully used in the 425A Micro-voltmeter and 412A VTVM, permits extremely low drift levels without any of the leakage current problems and attendant offset which plague other types of solid-state choppers. The new amplifier combines the photoconductor with a neon oscillator light source to provide a completely solid-state device with the ensuing advantages of long life, very low power consumption, and small size; and a drift level of one microvolt per week! Further, the chopping frequency is completely independent of line frequency, thus eliminating the problem of 60 cps and its harmonics producing dc offsets. To complement the low level capabilities of the photoconductor chopper, careful attention to layout and use of high quality insulating materials has been necessary to achieve microvolt zero stability under adverse environmental conditions such as high humidity.

**CHOPPER AMPLIFIER**

In an operational amplifier it is desirable to have the gain of the drift-free chopper amplifier as high as possible to reduce the effective drift of the main amplifier, and to make the dc loop gain very large. The gain is limited, however, by the fact that the chopper amplifier must go through gain crossover (0 db

---

1. John M. Cage, "An Increased-Sensitivity Micro Volt-Ammeter using a Photoconduc-
2. Donald Norgaard, "A Precision DC Vacuum-
Tube Voltmeter with Extended Sensitivity and High Stability," Hewlett-Packard Jour-
specifications

**Dymec Model DY-2460A Amplifier**

Open-loop Gain (Inverting): 5x10^6 at dc; 7-x10^6 at 40 cps; 1 at 1 kHz; values are maximum, 10°, 20°, and 30° load impedances >10K.

1. Comparator Input Impedance: 1M at dc; 150K at 1K, minimum values. Shunt capacitance 60 pf max.

2. Comparator Output Impedance: 1K ohms max from dc to 10 kHz; 50 ohms applied gain.

3. Comparator Input Noise: 4 mV p-p max, 0 to 10 cps; 10 mV rms max, 0 to 1K; values referred to summing point to ground. 0.5% of gain.

Zero Drift Constant Temp: 1 mv/week max. Temp Coeff: 0.5 mV/°C max. Values referred to summing point (24 hr. warm-up). Sum point to ground. <100K.

Zero Adjustment: ±20 mV referred to summing point.

Chopper Frequency: 190 to 300 cps, non-synchronous.

DC Output Capability: Voltage: ±10V.

Current: ±10 mA; values for range from dc to 10 kHz, 6 db/octave decrease from 1K to 1Kc.

Overload: Amplifier Limiting: +10.5 to +11.5V output. Recovery: Equal to rise time plus 20 μs. (5 ms max to sum point).

Overload Limiting: +10.0 to +10.5V threshold. Overload Signal: +15V overload, at rear connector, 5 ma available. (With Option B, only +10V)

Output Load: Max Capacity Load for Stability: 0.1A, if gain > 10; 0.01A if gain < 10. Short Circuit: Does not damage instrument.

Reactor: Control: Following circuit connections provided at rear connector. (Mating Connector listed under DY-2461A Plug-ins).


**DY-2461A-M1 Data Systems Plug-In**

Gain (Inverting): Fixed Settings: 10, 30, 100, 300, 1000 (×0 position shorts output).

Adjustment: 0% on each range. (Front panel screwdriver control).

DC Gain Accuracy: ±0.3%, ±0.6%, ±1.3%, ±2.5% (whichever is less).

Output: 500 milliamps max, 0 to 15V; 0.1A max. (whichever is less).

Gain: ±0.01% per week at constant temp. ±0.01%/°C max. Temp range 0 to 55°C.

DC Linearity: ±0.01% at any gain setting.

Input Resistance: 50 pf nominal. Maximum: Input, 300V peak or 220V rms (whichever is less).

BANDWIDTH AND SETTLING TIME: (Signal must be within output capability; see DY-2460A spec.)

Minimum Maximum 3 dB Settling Time

Gain 10 Bandwidth to 0.1% 10 10 30 300 1000

2. Filler Panel: For use with Combining Case. Covers one unoccupied panel opening. Stock No. 5660-0792, $3.00 each.

3. Control Panel Cover: For use with Combining Case. Covers all amplifiers, including carrying handle. Stock No. 5660-0808, $2.00 each.

Options: Overload Indication: Front panel lamp indication and output signal, provided under overload conditions. Order DY-2460A-M1, $430.00.

Price: DY-2460A Amplifier (less plug-in), $395.00.

**DY-2461A-M3 Patch Unit Plug-In**

Patch panel provides connections for up to 3 inputs and 1 feedback path. Inputs, output, circuit ground and chassis ground available at both front panel and rear connector. Summing point available at front panel only. Overload signal at rear only. ACCESSORIES AVAILABLE: Mating Rear Connector (not required if Combining Case used). Stock No. 9300-0004, $7.00 each.

Price: DY-2461A-M3 Patch Unit Plug-In, $75.00. Combined with DY-2460A Amplifier, $470.00.

**DY-2461A-M4 Plus-One Gain Plug-In**

Gain: <0.005% into 1kΩ; 0.002% into 100kΩ, Long Term Linearity, ±1.0% to 55°C.

AC Gain Accuracy: ±1.0% into 100kΩ at 40°C.

Bandwidth: (Signal must be within output capability; see DY-2460A spec.) 0.1A at 5K; 1A at 300K.

Input Resistance, 10° ohms, for relative humidity up to 70% at 40°C.

Input Capacitance: 50 pf nominal (reduced to 5 pf nominal if connection to rear connector removed).

Output Resistance: 50 milliamps max.

Bandwidth and Settling Time: (Signal must be within output capability; see DY-2460A spec.)

Minimum Maximum 3 dB Settling Time

Gain 10 Bandwidth to 0.1% 10 10 30 300 1000


Price: DY-2461A-M3 Patch Unit Plug-In, $75.00. Combined with DY-2460A Amplifier, $470.00.

**DY-2461A-M2 Bi-Phase Plug-In**

Gain (Inverting): Fixed Settings: 1, 10, 100, 1100, 11000 (×0 position shorts output). Vertrim Extend gain for each setting to 11, 110, 1100, 11000 respectively.

DC Gain Accuracy: ±1.0% at 1K; 0.67% at 10K; 0.67% at 100K; 0.67% at 1M; 0.67% at 1G; 0.67% at 1T (with 1% overload signal at rear only). (For 0.01% use 1.3.)

Chopper Intermodulation Distortion: Less than 0.2% of reading at gain >10, over frequency range 100 to 300 cps.

ACCESSORIES AVAILABLE: Mating Rear Connector (not required if Combining Case used). Stock No. 9300-0005, $14.00 each.

ACCESSORIES FURNISHED: Four Component Plugs, stock No. 8050-0105.

Price: DY-2461A-M2 Bi-Phase Plug-In, $125.00. Combined with DY-2460A Amplifier, $470.00.

Price: DY-2461A-M3 Patch Unit Plug-In, $75.00. Combined with DY-2460A Amplifier, $470.00.


Data subject to change without notice.

**Dymec**

Division of Hewlett-Packard Co.
395 Page Mill Road
Palo Alto, Calif.

THE new -hp- 3550A Portable Test Set, designed specifically for transmission line testing, will find wide use in alignment and maintenance of multichannel communication systems. The test set consists of a wide-range oscillator, an electronic voltmeter, and a patch panel containing attenuators and line-matching transformers. The battery-operated instruments are completely transistorized, contributing to the light weight and compactness of the set.

The 30-pound weight is a distinct advantage when the set is to be hand-carried into the field or into awkward to reach places, such as airplane structures or isolated telephone repeater stations. The rugged aluminum case is splash proof since no vent holes are required for the small amount of heat generated by the transistorized instruments (Figs. 1 and 4).

The oscillator and voltmeter operate from internal rechargeable batteries, or from a 115/230 volt ac line which also charges the batteries automatically. With batteries fully charged, the Portable Test Set may be operated continuously for at least 40 hours.

The HO-204B audio oscillator used in the test set is a rechargeable version of the familiar -hp- 204B battery-powered RC oscillator. This oscillator covers a frequency range from 5 cps to 560 kc with an output power of 10 milliwatts (2.5 v rms) into a 600 ohm load. Frequency accuracy is ±3% while the amplitude/frequency response is ±3%, which enables frequency response measurements to be made without monitoring and continually resetting oscillator output voltage.

The included 403B transistorized ac voltmeter is a new, versatile, general purpose instrument designed for laboratory and field use. Its frequency range is 5 cps to 2 Mc with full scale voltage ranges from 1 mv to 300 v and a db range from -72 to +52 dbm. Accuracy is within ±2% of full scale over a temperature range of 0°C to 50°C for frequencies between 10 cps to 1 Mc. This accuracy is traceable to -hp-'s own individually calibrated meters. A floating input permits isolated ground measurements up to a maximum of 500 v dc.

The heart of the Portable Test Set is the Model 353A Patch Panel, which adapts the oscillator and voltmeter to specialized transmission line testing. The patch panel has input and output sections which act as source and receiver for the transmission line.

The output section has an attenuator and impedance matching transformers which match the oscillator's 600 ohm output impedance to line impedances of 135, 600, and 900 ohms. The 135 ohm impedance level is associated primarily with carrier system testing while the 600 ohm impedance is for long distance and high quality program lines; the 900 ohm impedance is for local subscriber loops. The center-tapped transformers are balanced to better than 40 db on the output windings.

The patch panel is diagrammed in Fig. 3. The oscillator signal passes through two cascaded T-section attenuators to the output (source)
transformer. One attenuator section attenuates the signal in 1 db steps, while the other provides 10 db steps for a total maximum attenuation of 110 db. Two transformers cover the wide frequency range involved, with transformer T1 operating from 50 cps to 5 kc while T2 is designed for use from 5 kc to 560 kc.

The input (receiver) section uses transformers identical to the output section, providing balanced input at impedance levels of 135, 600, and 900 ohms in addition to a bridging impedance (10 k). In all positions except bridging, the voltmeter reads across the 600 ohm load in the transformer.

Only 7” of vertical panel space in a 19” rack (Fig. 1).

To facilitate servicing, the amplifier and power supply are built on three printed circuit boards which are accessible from both sides while operating. No internal adjustments are used on the amplifier, the front panel zero and gain being the only controls. In order that ground loop currents may be reduced to a minimum, the circuit ground is floating from the case with both grounds brought out to the rear connector.

The self-contained power supply is fully solid-state and draws less than 4 watts under maximum loading conditions. The voltages to the amplifying stages are regulated which, with the large amount of feedback inherent in the amplifier, makes the device virtually insensitive to line variations.

**ACKNOWLEDGMENT**

The design work was done in the Advanced Research and Development Division of the Hewlett-Packard laboratories by Albert J. Reichner and the undersigned, with some initial circuit design by John H. Caldwell. Tom Deaver performed the mechanical design, and Richard Y. Moss of Dymec transferred the instrument from the lab into production at Dymec.—Robert J. Strehlow
former secondary so that it reads dbm directly regardless of line impedance. In the bridging position, the transformer has a 1:1 turns ratio so that the voltmeter reads input voltage directly (the dbm scale then is correct only for 600 ohm lines, a correction factor being applied for other line impedances).

Switch S1 changes the transformers in both the input and output sections for the two frequency ranges involved. The 5 kc break point corresponds to the range switch on the oscillator. Switch S4, Meas-Cal, connects the input and output terminals together to allow setting a reference level on the voltmeter. In this manner, the insertion losses of the transformers are accounted for.

Insertion loss and frequency response measurements are made easily with the 3550A Portable Test Set. Fig. 6a illustrates the connection between the Test Set and a telephone transmission line when no dc voltage is present on the line. Fig. 6b illustrates the connection between the test set and a telephone line with dc voltage present. The transformers in the patch panel are not designed for dc current, so that holding coils and blocking capacitors are used in this situation. The insertion loss of the holding coils may be calibrated out, where a transmission line loop is being measured, by shorting the input end of the line to the output end.

The design team for the Model 3550A consisted of Noel M. Pace, Robert B. Moomaw, Gale C. Hammeiwright, and the undersigned, at the Loveland Division of the Hewlett-Packard Company.

—Don A. Wick

### SPECIFICATIONS

**-hp-**

**MODEL 3550A**

**PORTABLE FREQUENCY RESPONSE TEST SET**

**OSCILLATOR (-hp- H07-204B)**

- Frequency Range: 5 cps to 560 kc
- Frequency Response: ±5% into rated load
- Output Impedance: 600 ohms
- Output: 10 milliwatts (2.5 v rms) into 600 ohms; 5 v rms open circuit; completely floating (isolated)
- Output Control: Continuously variable bridged "T" attenuator, to 40 db.
- Distortion: Less than 1%
- Hum and Noise: Less than 0.05%
- Temperature Range: −20°C to +50°C
- Power Supply: 4 rechargeable batteries (furnished), 40 hour operation per recharge (20 hours at −20°C), up to 500 recharge cycles. Self-contained recharge circuit functions automatically when instrument is connected to ac line (115 or 230V ±10%, 50 to 1000 cps); approximately 3 watts
- Dimensions: 6-3/32 in. high, 5¼ in. wide, 8 in. deep
- **VOLT METER (-hp- 4038-DB)**
  - Range: 0.001 to 300 volts rms full scale (12 ranges) in 1, 3, 10 sequence. −75 dbm to −52 dbm
  - Frequency Range: 5 cps to 2 mc.

**ACCURACY:**

- 0°C to +50°C: 5 to 10 cps: +5%  
- 10 cps to 1 Mc: ±2%  
- 1 to 2 Mc: ±5%  
- 0°C to −20°C: 5 cps to Mc: ±8%

**METER:**

- Minimum reading to average value of input waveform and is calibrated in dbms of a sine wave
- Nominal input Impedance: 2 megs shunted by approximately 50 pf on 0.001 to 0.03 volt ranges, 25 pf on 0.1 to 300 v ranges
- Overload Protection: Fuse protected
- DC Isolation: Signal ground may be −500 vdc with respect to instrument case

**TEMPERATURE RANGE:**

- −20°C to +50°C
- 50 cps to 560 kc.

**POWER SUPPLY:**

- 4 rechargeable batteries and recharge circuit same as H07-204B oscillator

**DIMENSIONS:**

- 6-3/32 in. high, 5¼ in. wide, 8 in. deep

**PATCH PANEL (-hp- 353A)**

- For Test Set and telephone line loop measurement
- Insertion Loss: Less than 3½ db at 1 kc.
- Accuracy: 100 db section: Error is less than ±0.35 db at any step.
- Attenuation: 110 db in 1 db steps
- Dimensions: 6-3/32 in. high, 5¼ in. wide, 8 in. deep

**OUTPUT:**

- Source: Frequency Range: 50 cps to 560 kc.
- Balance: Better than 4 db.
- Frequency Response: ±½ db, 50 cps to 560 kc.
- Impedance: 135, 600, and 900 ohms center-tapped
- Insertion Loss: Less than 1½ db at 1 kc.
- Distortion: Less than ½%, 50 cps to 560 kc.
- Maximum Level: +10 dbm (2.5 v rms at 600 ohms).
- Dimensions: 8H in. high, 19V4 in. wide, 13¼ in. deep (with cover installed)
- Weight: Net 30½ lbs., shipping 45 lbs.

**PRICE:**

- -hp- 3550A Test Set, $990.00.
- Prices f.o.b. factory

Data subject to change without notice.